



11th ARL/USMA Technical Symposium



ANALYTICAL DETERMINATION OF SHOCK RESPONSE SPECTRA, FOR A PROPORTIONALLY DAMPED SYSTEM

R. David Hampton & Nathan S. Wiedenman
Department of Civil & Mechanical Engineering
U. S. Military Academy, West Point, NY

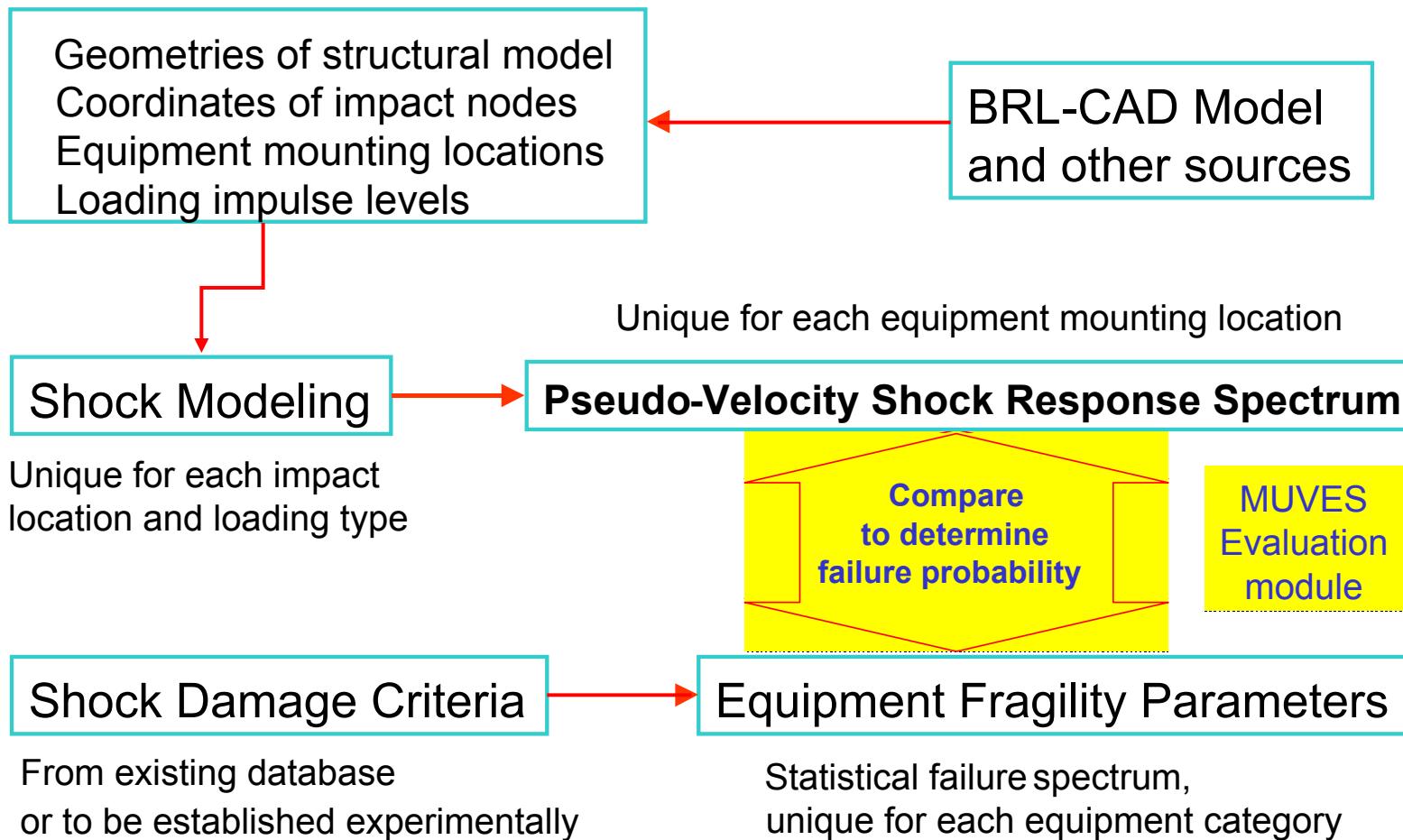
Ting H. Li
Weapons & Materials Research Directorate
U. S. Army Research Laboratory, Adelphi, MD

05 November 2003



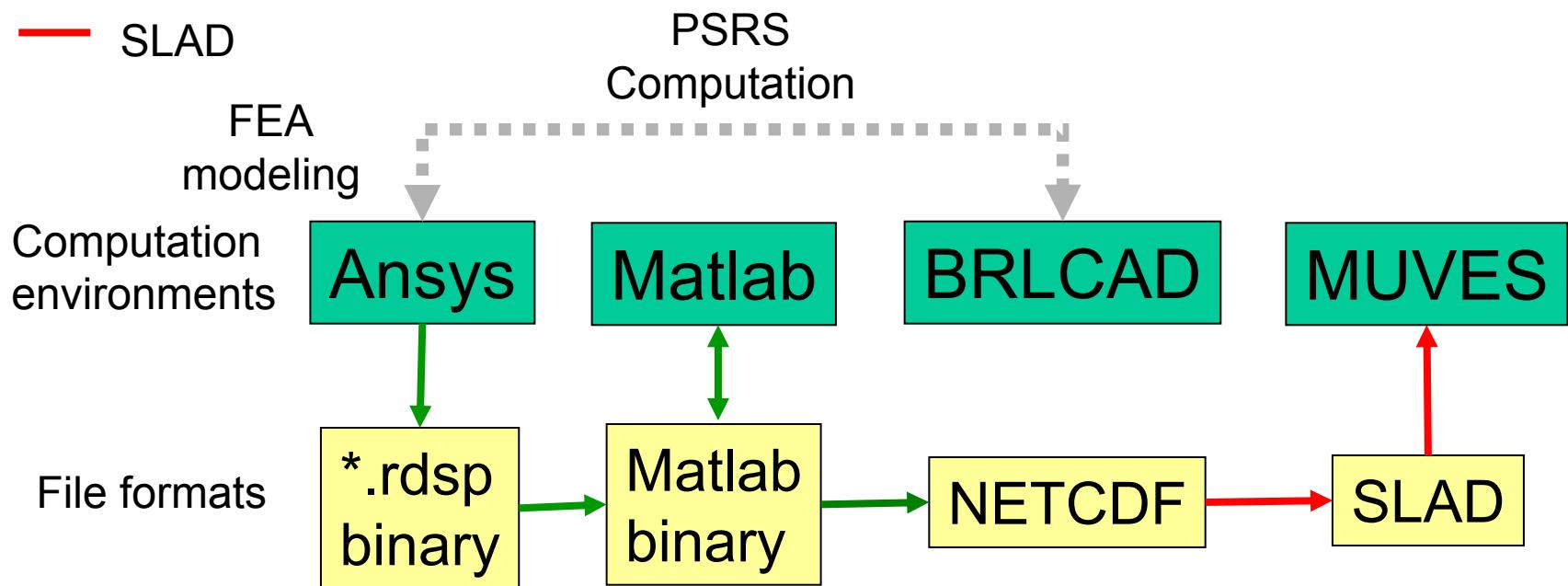
WMRD-CLSB

SLAD





- WMRD
- SLAD



- Different computational environments need to communicate with each other by correct file conversion.
- To handle large amounts of data better, conversion codes are being rewritten to improve efficiency.

FEA Shock Models for Armored Vehicles: Reducing the time for impact calculations



$$[M] \ddot{\{x\}} + [C] \dot{\{x\}} + [K] \{x\} = \{F\}$$

FEA
Structural
Transient
Analysis

Direct Integration

- Used by most analysts
- Current shock model: ~2 days/impact
- Too slow for many impacts
- But can be used for comparison in a few cases

Modal superposition

- Very fast for large number of impacts
- For linear system only (based on linear superposition of modes)
- Clear-cut upper frequency, which is limited by number of modes; possible in eigen analysis

Explicit

Implicit

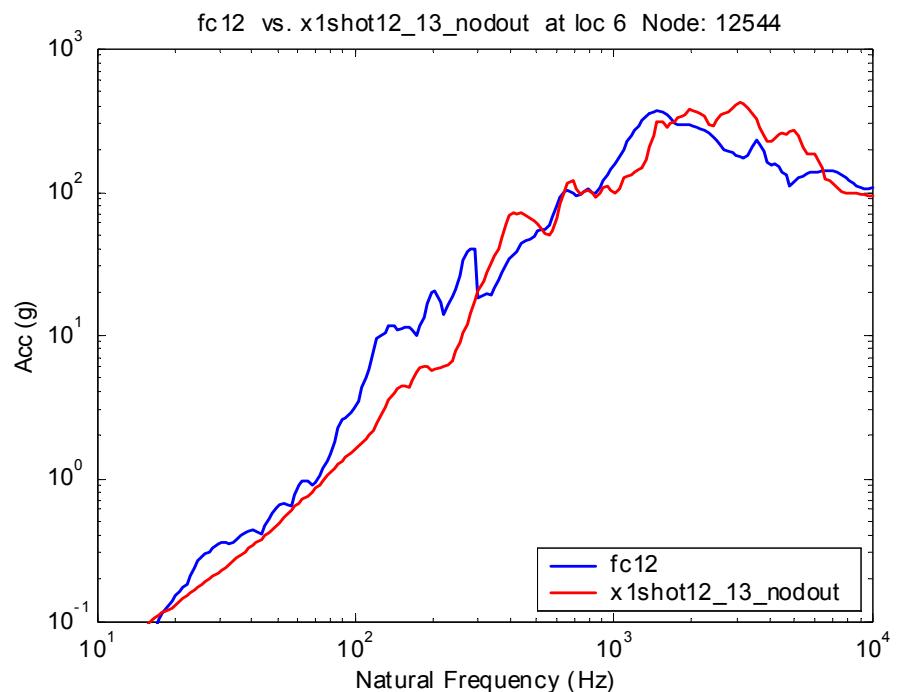
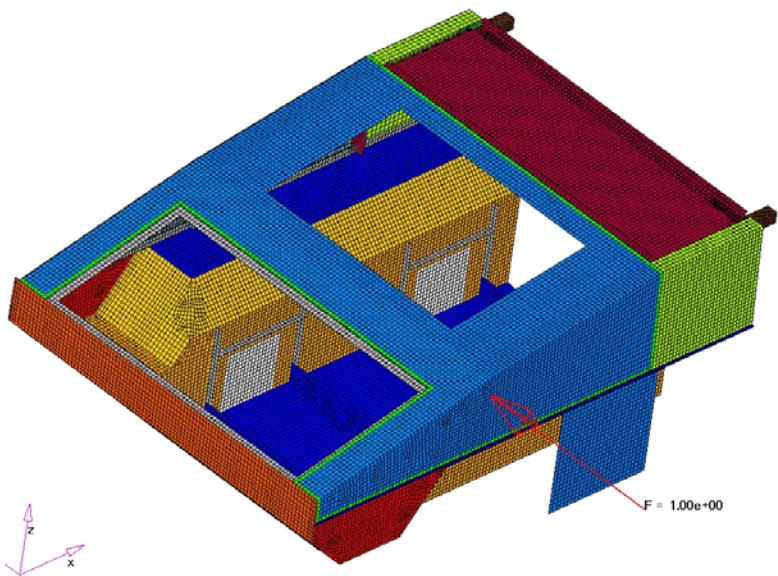
Dyna
Abacus

Nastran
Ansys

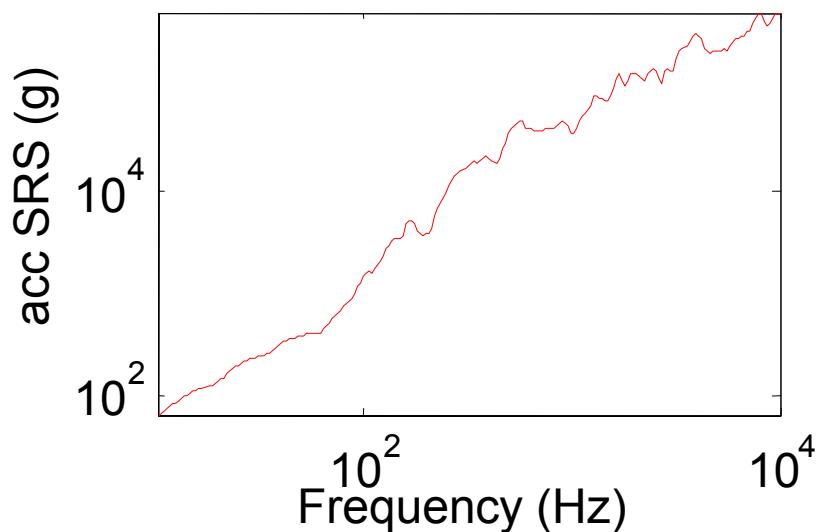
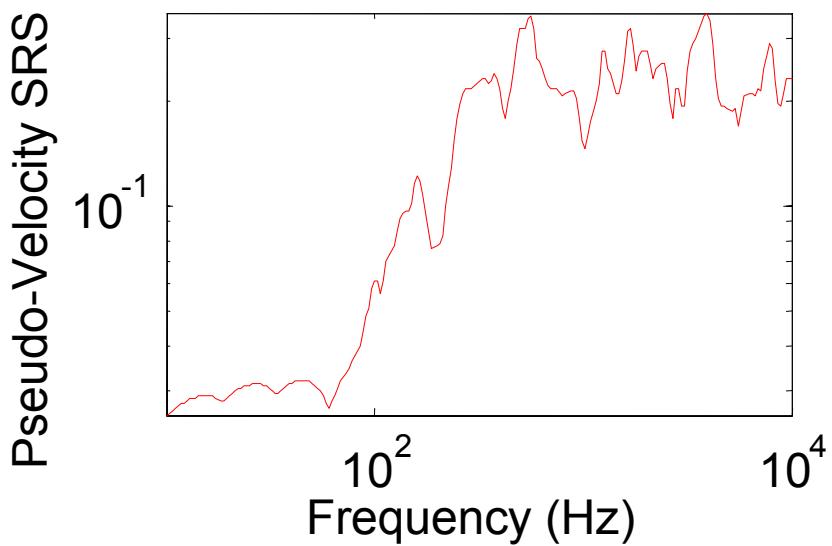
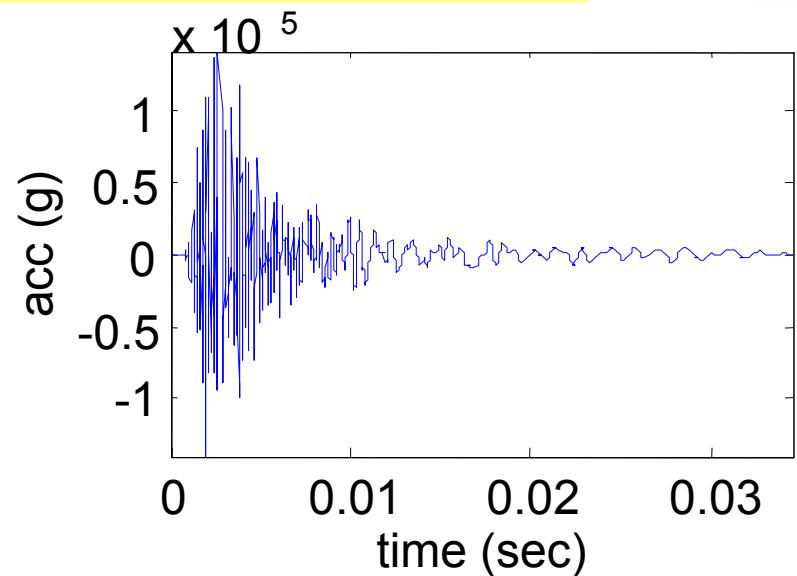
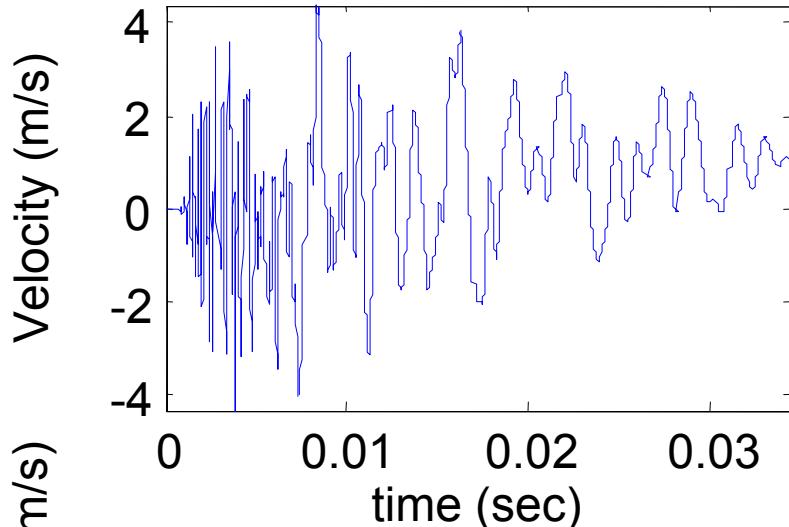
Ansys

FCS-X1 shock model

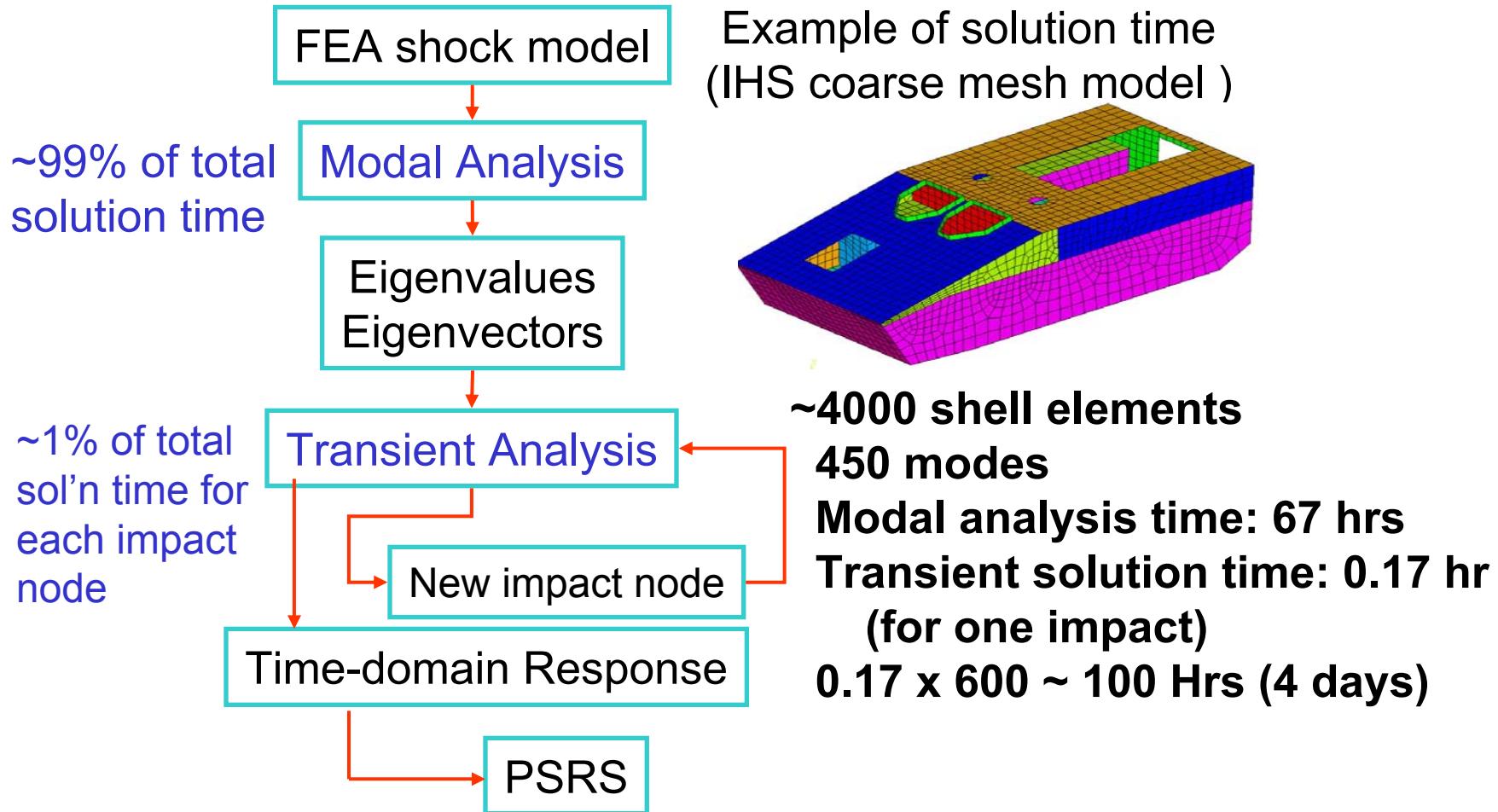
Blue: Shock response measurement from ballistic test
Red: Corresponding response from a FEA shock model



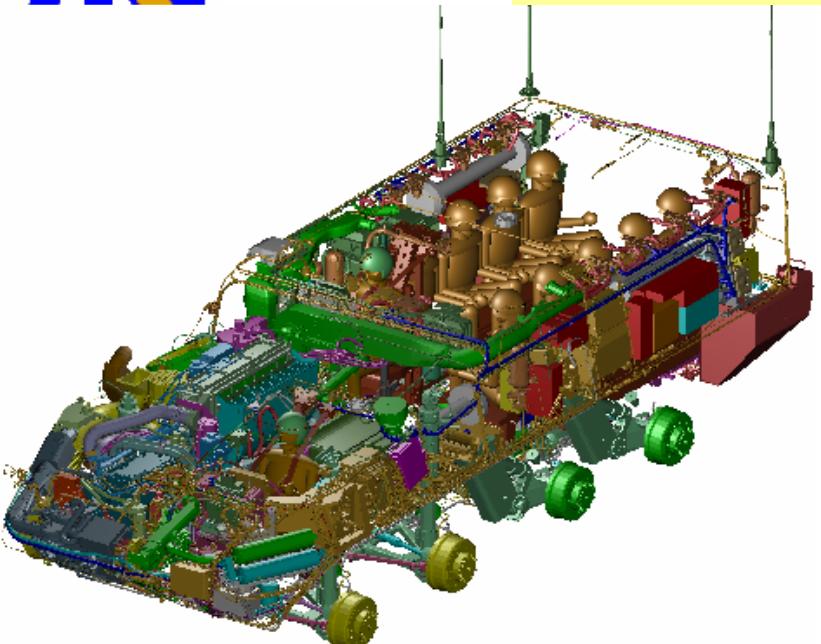
Typical SRS Data and Plots



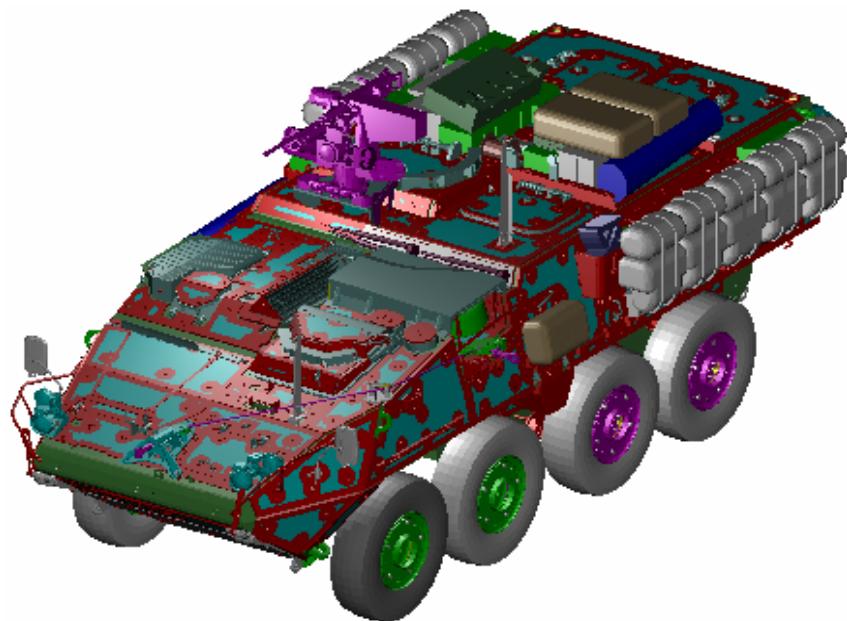
FEA Modal Superposition Method



Stryker BRLCAD Model – Basis for the FEA Model



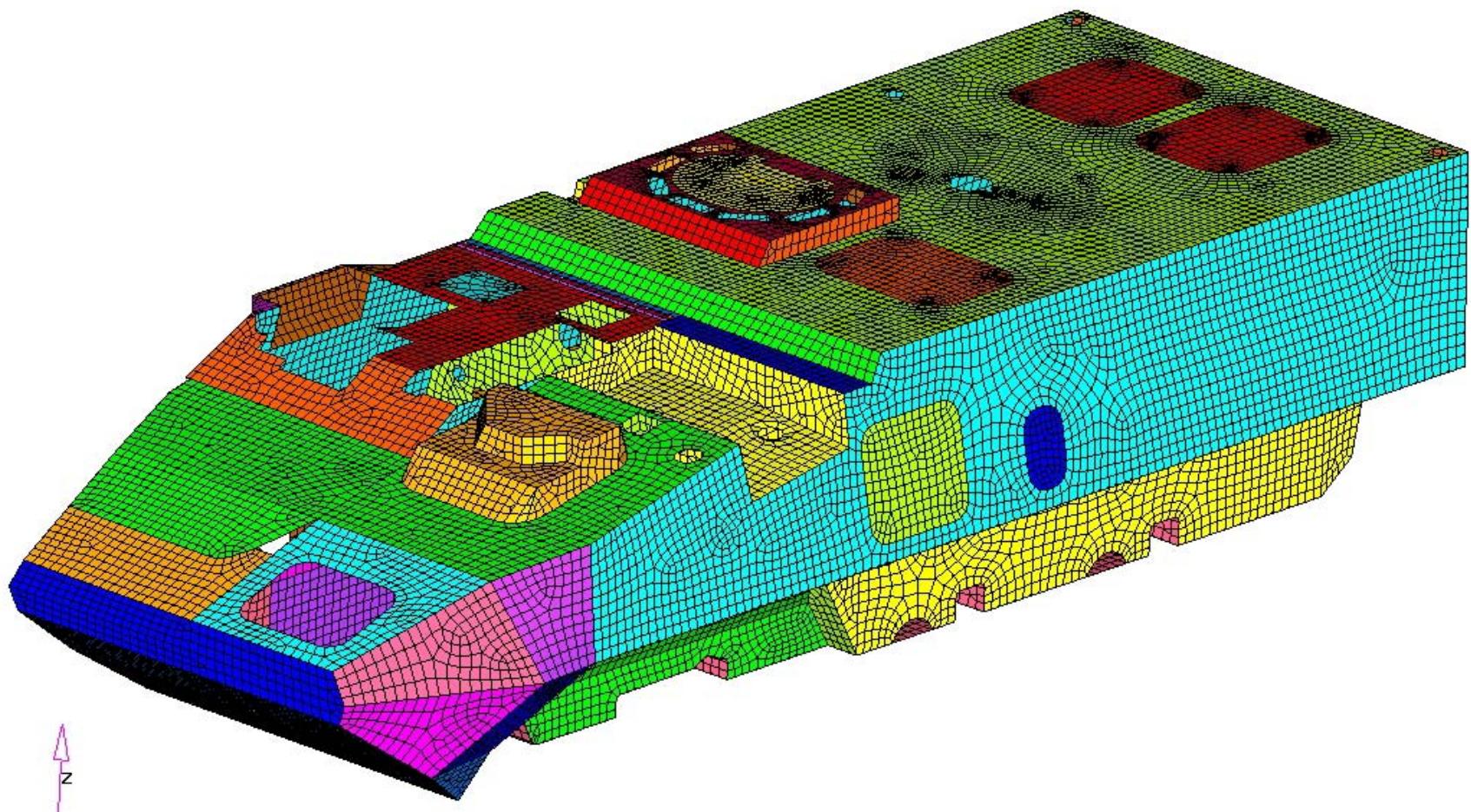
Interior Components



Exterior Components

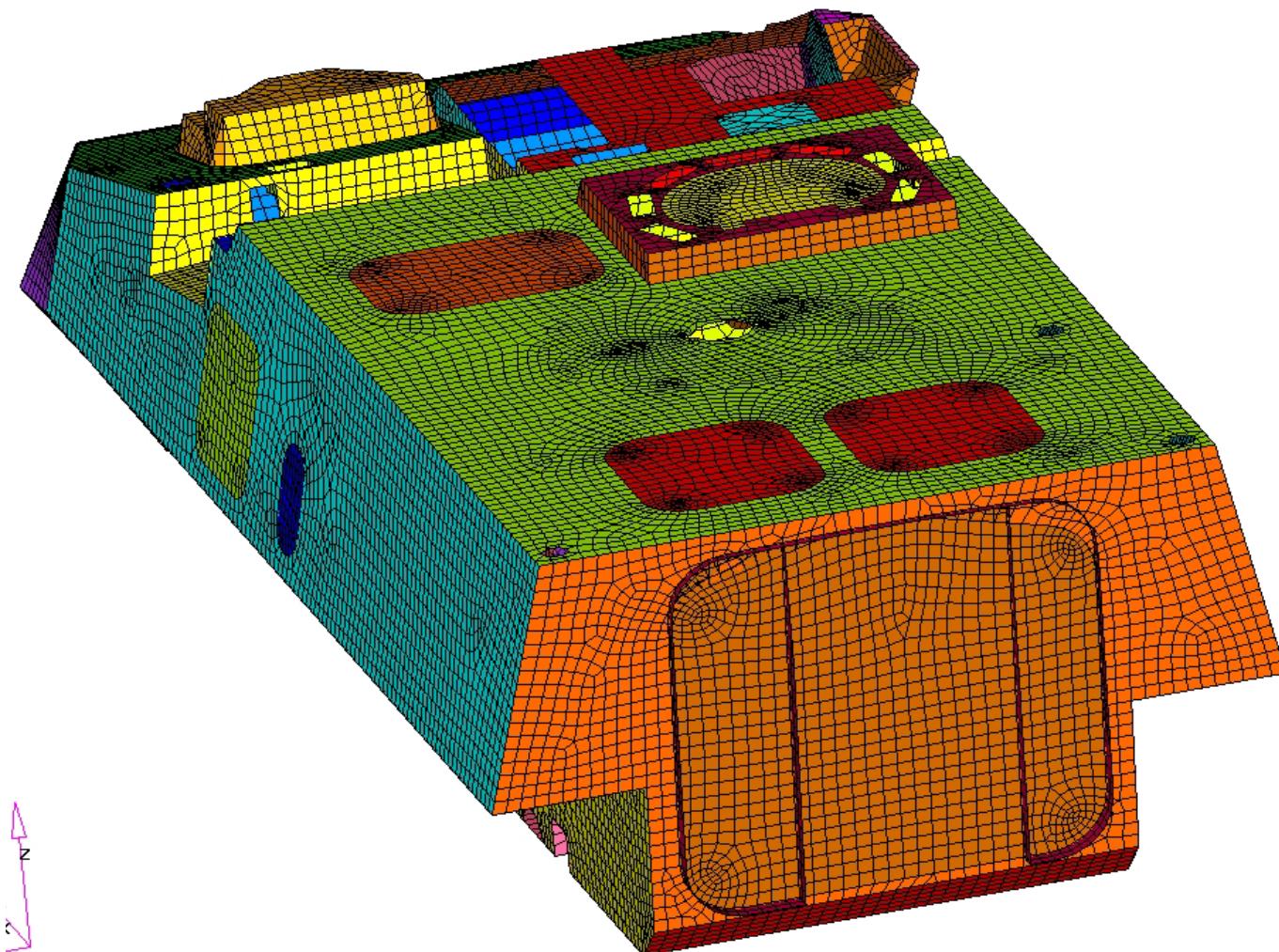


Stryker FEA Model

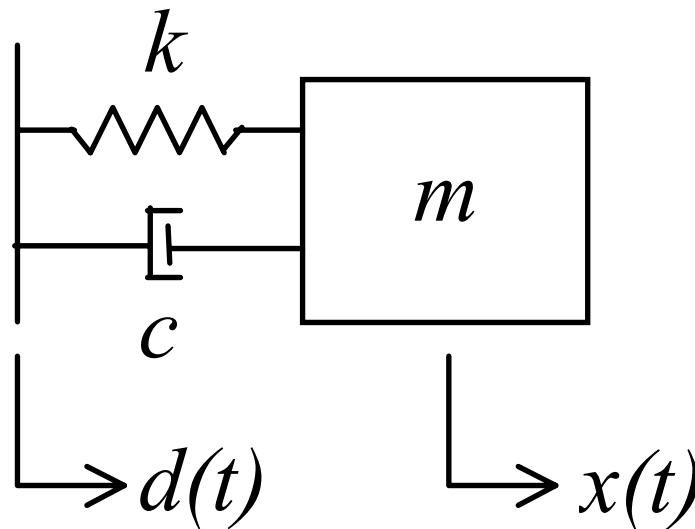




Stryker FEA Model



RESEARCH OBJECTIVE: Analytical SRS Determination



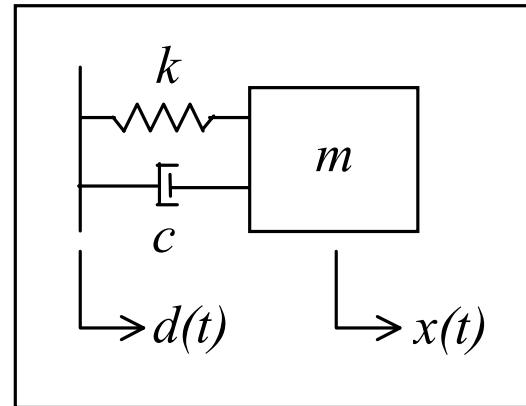
Hypothetical SDOF MSD system,
for SRS determination



SRS Definitions:

Spectral displacement SRS:

$$S_D(\omega_n) := |x(t) - d(t)|_{\max}$$



Spectral velocity SRS:

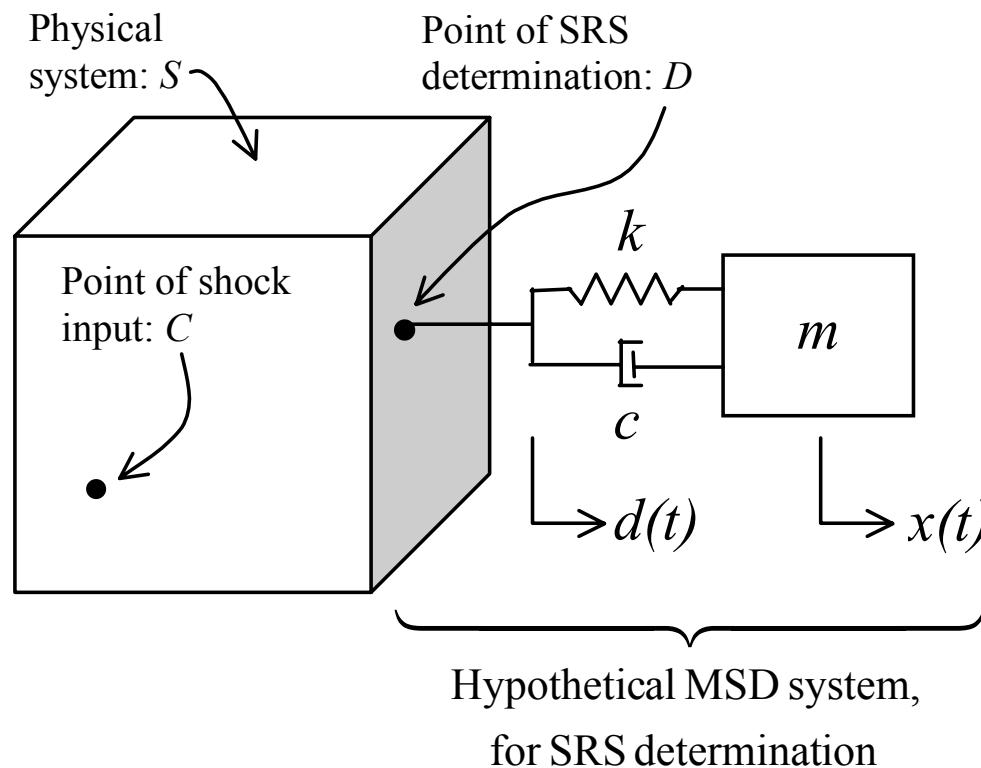
$$S_V(\omega_n) := \omega_n |x(t) - d(t)|_{\max} = \omega_n S_D(\omega_n)$$

Spectral acceleration SRS:

$$S_A(\omega_n) := |\ddot{x}(t)|_{\max}$$



Linear system model:

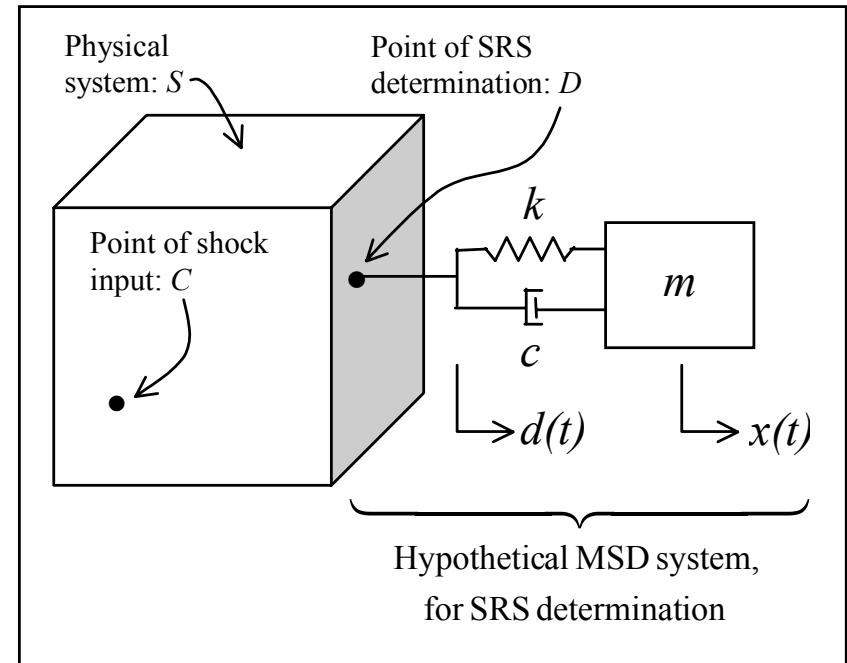




USING LINEAR MODEL

Disturbance $d(t)$:

$$d(t) = \sum_{i=1}^v d_i(t)$$



$$d_i(t) = D_i e^{-\alpha_i t} \sin(\omega_i t + \phi_i) u_{-1}(t)$$

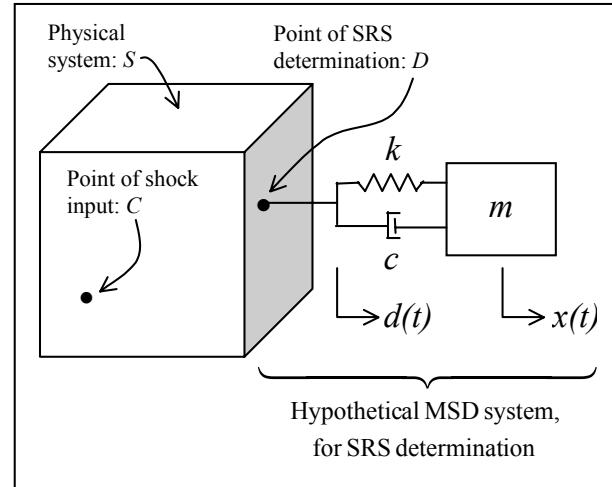


SOLUTION

Displacement $x(t)$:

$$x(t) = \beta e^{-\zeta \omega_n t} \sin(\omega_d t + \psi)$$

$$\begin{aligned}
 &+ \gamma \sum_{i=1}^v D_i \left\{ e^{-\zeta \omega_n t} [\delta_{1i} \sin(\omega_d t + \phi + \phi_i + \theta_{1i}) \right. \\
 &\quad \left. + \delta_{2i} \sin(\omega_d t + \phi - \phi_i + \theta_{2i})] \right. \\
 &\quad \left. + e^{-\alpha_i t} [\delta_{3i} \sin(\omega_i t + \phi_i + \theta_{3i})] \right\}
 \end{aligned}$$





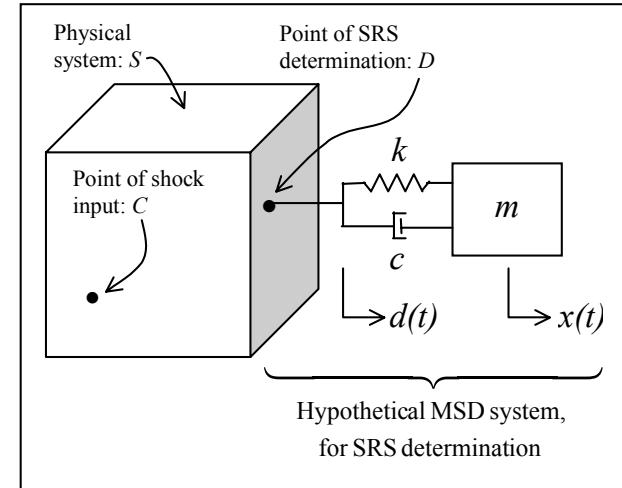
SOLUTION

Relative Displacement:

$$\delta(t) = x(t) - d(t)$$

$$= \beta e^{-\zeta \omega_n t} \sin(\omega_d t + \psi)$$

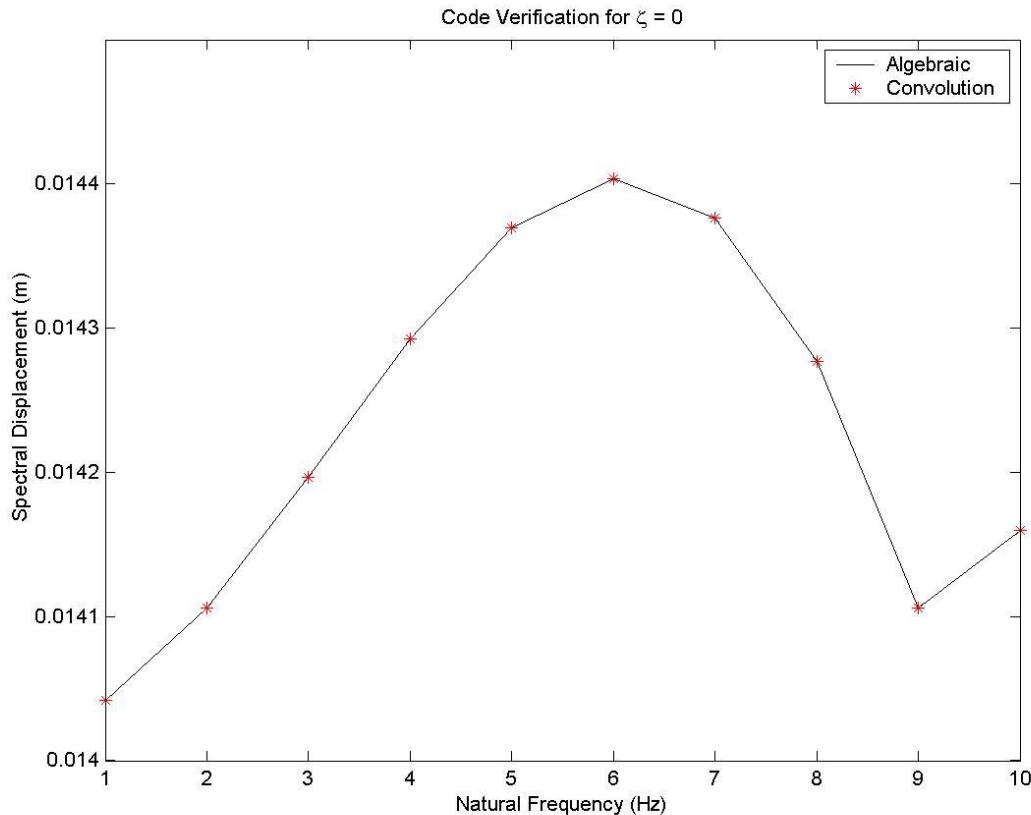
$$\begin{aligned}
 &+ \gamma \sum_{i=1}^v D_i \left\{ e^{-\zeta \omega_n t} \left[\delta_{1i} \sin(\omega_d t + \phi + \phi_i + \theta_{1i}) \right. \right. \\
 &\quad \left. \left. + \delta_{2i} \sin(\omega_d t + \phi - \phi_i + \theta_{2i}) \right] \right. \\
 &\quad \left. + e^{-\alpha_i t} \left[\delta_{3i} \sin(\omega_i t + \phi_i + \theta_{3i}) \right. \right. \\
 &\quad \left. \left. - \sin(\omega_i t + \phi_i) / \gamma \right] \right\}
 \end{aligned}$$





- Algebraic results used to generate Shock Response Spectra, via MATLAB code
- Implementation verified for small range of frequencies, undamped case:
 - By hand for algebraic results
 - Using MATLAB to calculate the convolution integrals

Code Verification



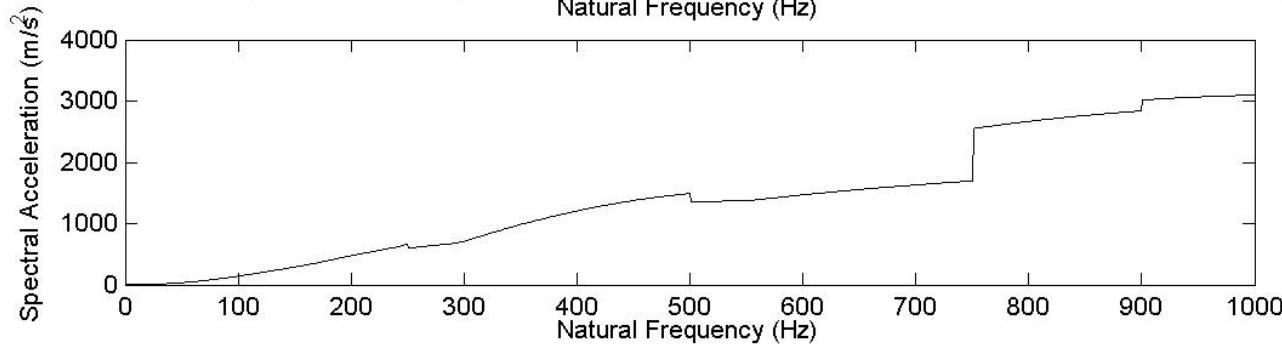
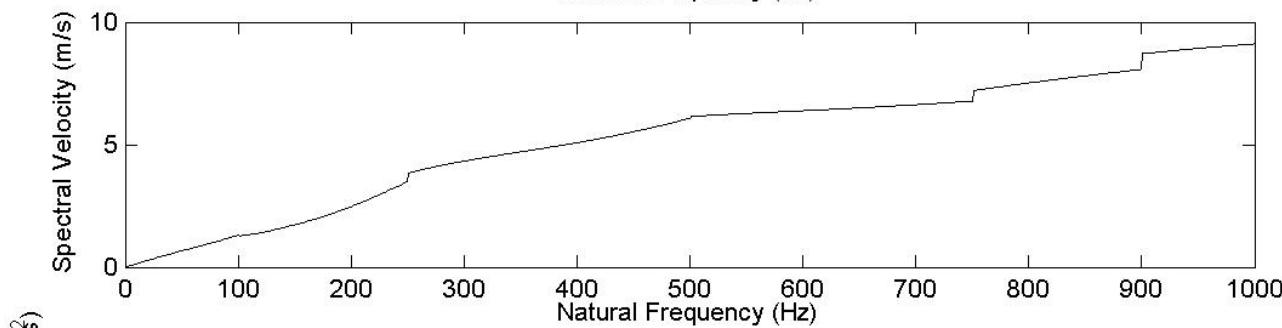
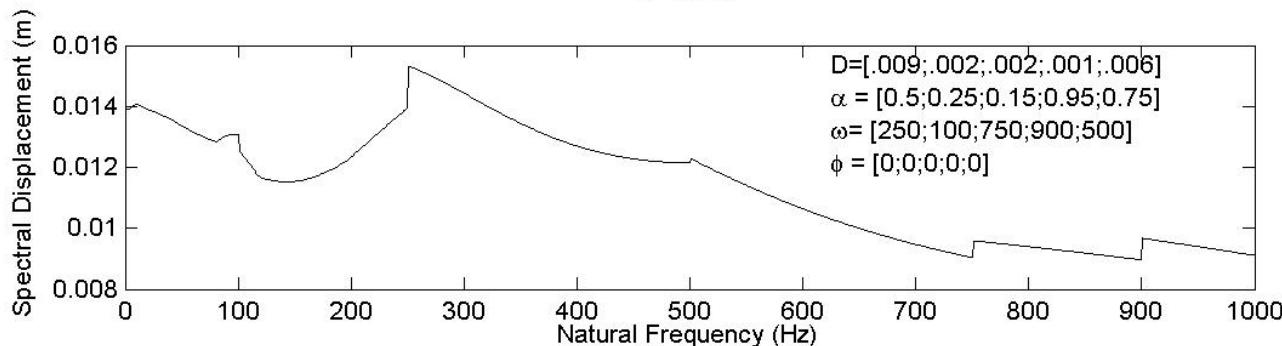
Natural Frequency	Algebraic solution data	Convolution solution data
1	0.01404178803909	0.01404178803909
2	0.01410566896492	0.01410566896492
3	0.01419624521110	0.01419624521110
4	0.01429238837489	0.01429238837489
5	0.01436953813222	0.01436953813222
6	0.01440384367614	0.01440384367614
7	0.01437636721478	0.01437636721478
8	0.01427672293821	0.01427672293821
9	0.01410558906370	0.01410558906370
10	0.01415993354654	0.01415993354654

-Numerical evaluation using convolution integrals
agrees with numerical evaluation using algebraic solution.

MATLAB Output



$\zeta = 0.707$





CONCLUDING REMARKS



- **New method developed for SRS calculation**
 - Does not require numerical evaluation of convolution integral
 - Exact for impulsive shock disturbance
 - Valid for linearized system model
- **Implementation achieved in MATLAB**
- **Calculations useful**
 - for evaluating other methods of SRS calculation*
 - for determining minimum number of modes required for SRS of specified accuracy*